ABSTRACT:
The production of bio-based chemicals and fuel from biomass is considered cleaner production technology for environmental protection. In the present study, establishing a new process to convert biomass to highly pure sugars and solid biofuel by concentrated acid hydrolysis was investigated. The sugar production process was based on two-steps concentrated H$_2$SO$_4$ hydrolysis of rice straw followed by separation and purification of sugars. Moreover, ethanol was separated from acids by using a distillation unit. The hydrolyzer unit can convert 10 kg/h rice straw to sugars, and their final yield was 1 kg sugars per batch. An economic method for separation of sugars by precipitation using ethanol and highly efficient acid recovery (90 %) and ethanol (95-98%) was achieved without using resins. High-performance liquid chromatography analysis for hydrolysate revealed that it contains 77% xylose, which can be used as natural diet sugars. The production of 70 -100 kg natural diet sugars and 700 kg solid biofuel (Calorific value of 6952 kJ/kg) were obtained from 1000 kg rice straw. The results from the pilot plant could be considered as a step towards the commercialization of the process.

Keywords: Biomass, edible sugars, solid biofuel, pilot-scale unit

1. INTRODUCTION

There are various biomass sources such as wood and wood wastes, crops, waste by-products, municipal solid wastes, animal wastes, waste from food processing, and aquatic plants and algae [1]. Because of the energy crisis, lignocellulosic biomass has emerged as a potential substitute for maintaining environmental sustainability. However, the conversion of biomass into value-added products still faces challenges in finding a proper unit operation. The cost-intensive of enzymatic system limits effective saccharification to hydrolyze the biomass and considered the stiff-necked of the process [2].

Green production technology for the alternative chemical and energy resource based on biomass has attracted increasing interest. However, their commercialization will require several technologies, such as low-cost feedstock. In Egypt, the agricultural residues are estimated to be over 35 million tons/year, and their disposal causes an environmental problem. For instance, rice straw causes black clouds. Plant-based materials containing cellulose are feedstocks that may be susceptible to acid or enzymatic hydrolysis [3]. There are several technologies available for the conversion of lignocellulosic. The main difference between these technologies is different catalysts used for the brake-down of polysaccharides in the raw material [4].

Fractionation of lignocellulosic materials by organosolv pretreatment is concerned in many types of research. The valorization of hemicellulose- and lignin-rich fractions for high-value applications are the main achievements of these researches. Organosolv-based processes are considered economically attractive due to their high solid pretreatment loadings and little water usage [5]. The fractionation of lignocellulosic material can be taking place by several convenient techniques. However, the use of strong acids and bases, high temperature and pressure requirements, and expensive instrumentation make the pretreatment methods challenging to use. Therefore, pretreatment techniques using greener solvents such as supercritical fluid, ionic liquid, and deep eutectic solvent (DES) can overcome these difficulties. But to apply the greener technologies commercially, many pilot-scale scales and more studies are mandatory [6].

Fractional hydrolysis is a novel process that used different inorganic acids to fully recover the number of fermentable sugars as separate fractions, direct from the biomass with minimum toxics generation for bioethanol production [7,8]. Supercritical water ultrafast hydrolysis of the cellulose fraction can be considered as the core of this process. The operation is a continuous system that should be a real alternative to removing lignocellulosic fractionation [9].

The vital step for the production of sugars and bio-based chemicals is the hydrolysis of lignocellulosic biomass. To measure the time-dependent formation of sugars (glucose, xylose, mannose), and furfurals, a semi-continuous plant with diluted sulphuric acid as a catalyst at different hydrolysis temperatures for three types of lignocellulose (hardwood, softwood, and grass) were studied [10].

Sugars’ recovery from agricultural biomass by the FASTSUGARS process was investigated on a pilot plant scale. It was found that the hydrolysis of
biomass was slow down by controlling particle size because large particle size acted as a mass transfer resistance. This slow hydrolysis resulted in lower conversion and reduced sugars' degradation yield by 15% lower in the pilot plant. Besides, higher selectivity to sugars was obtained [11]. The xylooligosaccharides (XOS) and fermentable sugars production from Miscanthus using steam explosion (S.E.) pretreatment was studied on a pilot plant scale. Enzymatic hydrolysis for both the XOS-rich hydrolysate and solid residues was applied to obtain fermentable sugars [12]. In the pilot-scale unit, oil palm as a renewable resource for bioethanol production was investigating [13], and modularizing bioethanol production from lignocellulose data was collected [14].

Crystalline cellulose and natural hemicellulose become utterly soluble in 72% H$_2$SO$_4$ or 42% HCL at room temperature. Since the polysaccharides' depolymerization favors the formation of oligosaccharides, nearly no monosaccharides are decomposed in concentrated acid. It is essential to appreciate that the cellulose chains dissolve in concentrated acid and then hydrolyze in a homogeneous reaction medium to oligomers [15]. The method of using concentrated sulfuric acid for biomass hydrolysis has many advantages. For instance, this method can be proceeded at low reaction temperature and little by-product, in addition to high yield. However, this method has the disadvantage of the high cost for acid recovery. Many researchers investigated an electrode dialysis method to recover sulfuric acid from the concentrated acid hydrolysate of plant cellulose material, but this method is high in running and capital intensive [16]. Afterward, new systems of recovering acid using strong acid cation exchange resins to adsorb sugars in the liquid portion were studied. However, this new system still has a disadvantage of the high recovery cost due to resins' low adsorption capacity [17].

A method for producing carbohydrates from plant cellulose material by concentrated sulfuric acid was studied [18]. The process was stopped at the middle before diluting the acid to a concentration between 20% and 30%. It was then mixing the concentrated acid main hydrolysate of plant cellulose material with a liquid organic precipitant, thus obtaining a sugar precipitate and an organic precipitant solution containing sulfuric acid. This method has many problems, such as low sugars yield, and the final product will be oligosaccharides, but not glucose.

A complete process for producing highly pure edible sugars and solid biofuel from rice straw was investigated on a pilot-scale in the present study. The concentrated acid hydrolysis was briefly achieved by using 70% acid concentration then diluted to 25% or 30%. Then, evaporating the optimum amount of water from hydrolysate to enable the sugars to precipitate. Besides, we use precipitant to decrease the solubility of sugars. At the end of the process, the precipitant is separated from acid by evaporation and condensation and reused. The study’s purpose was to establish a new technique to determine the potential amount of sugar and solid biofuel production from 1000 kg rice straw; based on the pilot-plant operation. Furthermore, the amount of acid and ethanol recovered from the batch process were calculated.

2. MATERIAL AND METHODS

2.1. Materials

The raw materials used were Rice straw; they were sun-dried and reduced in particle size to be suitable for handling. The chemicals used are 98% sulfuric acid of industrial grade and 95% ethanol and lime, purchased from El-Gomhouria Pharmaceuticals and Chemicals Company, Cairo, Egypt.

2.2. Equipment

Hydrolyzing tank (iron tank lined by polyvinylidene difluoride (PVDF)); fire source; stainless steel screener (with cheesecloth made from polyester); plastic clarifier; separator for acid and alcohol (batch distiller with a 5 K.W. heater) and spray dryer.

2.3. Procedure

2.3.1. Hydrolysis reaction

A 70% sulfuric acid solution was prepared and mixed with rice straw (solid: liquid ratio, 1: 1) with manual intermittent agitation (for the 15-minute interval) and at 60-70°C for 20 min., followed by water addition to reaching the acid concentration to 25% and heating at 100 °C for 1 h.

2.3.2. Separation process

After the hydrolyzation process, the solid fraction, mainly lignin, was separated from the hydrolysate using a cheesecloth screener. Then the hydrolysate transfer to a clarifier to settle the particles down. Experimental work was done to compare filtration and sedimentation, and it was found that sedimentation was more effective, easy, and cheaper. Also, the long residence time during filtration may increase the solubility of sugars in ethanol and lead to high losses of sugars in the ethanol stream, therefore, decrease the final yield of sugars.

2.3.3. Concentration and separation of sugar from hydrolysate

The Concentration of hydrolysate was taken place by evaporation of 10,20,30,35,38,44 % volume/volume hydrolysate to determine the optimum percent removal of the solution before the sugars being burned. The addition of ethanol to the solution was 2-3 times the hydrolysate volume. Then, separation of the liquid phase (acid and alcohol) from the sugars followed by washing the sugars with ethanol, and the remaining amount of ethanol was evaporated. The sugar solution was neutralized by lime and using a spray dryer to
separate sugars. Finally, a liquid phase that contains acid and alcohol was evaporated to separate and recover both alcohol and acid from being reused in the process.

2.3.4. Preparation of silica from solid residues
From rice straw and cotton gin trash, which contain high amounts of silica, silicic acid was extracted from the solid residues using 5%–10% sodium hydroxide. Concisely, the solids were heated, pressed, and washed with water to remove a liquid. Reduce the liquid's pH by treating with acid, thus, creating a separated residue, preferably by filtration. Pure silica can be obtained by bleaching and can be further treated to produce sodium silicate, potassium silicate, or other useful materials.

2.4. Analysis
The sugar concentration was determined as total reducing sugars by the phenol-sulfuric acid method [19], by Fehling analysis method [20], and the hydrolysate sugars composition by High-Performance Liquid Chromatography (Hewlett-Packard Liquid Chromatograph Series 1050 with R.I. detector using Bio-Rad Aminex HPX-87C column 300mm x 7.8mm and deionized water as mobile phase, injection volume of 15μl at 70°C with a flow rate of 0.6ml/min) at Central – Labs, Egyptian Petroleum Refinery Institute. The Gross calorific value (K.J./kg) of three samples of the solid residues, main lignin from three different experimental runs, was determined according to ASTMD 240 using Tarr 200 calorific value tester at Central – Labs, Egyptian Petroleum Refinery Institute. The silica was determined by NICOMP 380 ZLS dynamic light scattering instrument (PSS, Santa Barbara, CA, USA) at Nanomaterial Investigation Lab., Central Laboratory Network, National Research Center, Cairo.

3. RESULTS AND DISCUSSION
3.1. Concentration and separation of sugar from hydrolysate
The hydrolysate was concentrated by solvent evaporation. The optimum removal of solvent was 38 % volume without burning sugar, which increased sugar concentration in hydrolysate from 16.46 to 27 %. Also, sugar should be washed with ethanol after separation to be free from furfural. Thus, sugar powder became very pure after two washing times, as shown in Figure 1.

Table 1. Quantitative analysis of sugar in hydrolysate and sugar powder

<table>
<thead>
<tr>
<th>The analysis method</th>
<th>% of sugar / biomass</th>
</tr>
</thead>
<tbody>
<tr>
<td>Phenol - sulfuric acid</td>
<td>38 % (g sugar / 100 ml hydrolysate)</td>
</tr>
</tbody>
</table>
Table 2. The composition analysis of sugars in hydrolysate by HPLC.

<table>
<thead>
<tr>
<th>Sugar type</th>
<th>Percent</th>
</tr>
</thead>
<tbody>
<tr>
<td>Xylose</td>
<td>77</td>
</tr>
<tr>
<td>Glucose</td>
<td>11.3</td>
</tr>
<tr>
<td>Arabinose</td>
<td>11.7</td>
</tr>
</tbody>
</table>

3.3. Quantitative analysis of the produced solid fraction (mainly lignin) and silica

The material balance for sugar production from rice straw was 700 kg, mainly lignin produced from 1000 kg rice straw. As shown in Table 3, the solid fraction (primarily lignin) has a mean gross calorific value of 6952 kJ/kg. Therefore, this solid fraction can be used as biofuel, which increases the process’s economy. Moreover, this solid fraction’s calorific value is close to bagasse, which has a gross calorific value of 9500 kJ/kg [23]. However, this solid fraction’s lower calorific value may be attributed to its high moisture and ash residues. The silica produced from the residue fraction after the hydrolysis of rice straw can be considered a valuable by-product with 99% of distribution > 1018 nm, as shown in Figure 2. The chemicals were recovered with 90% and 95 – 98% for sulfuric acid and ethanol to achieve maximum economy. The losses of acid may be due to the gaseous fumes (mainly SO₃ and CO₂) that evolved during the hydrolysis process. Therefore, using an absorption unit connected to the gaseous fumes’ outlet for pollution control is recommended. Also, much amount of water can be recovered from evaporation processes and reused.

Table 3. The gross calorific value of the produced solid fraction (mainly lignin) kJ/kg *

<table>
<thead>
<tr>
<th>Sample ID</th>
<th>Results</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>6873</td>
</tr>
<tr>
<td>2</td>
<td>7267</td>
</tr>
<tr>
<td>3</td>
<td>6716</td>
</tr>
</tbody>
</table>

*Test was made according to ASTMD – 240

3.4. Design part

The previously discussed economic method was used to construct a pilot plant unit in the present study. Figure 3 shows the flow sheet for the production of edible sugars and solid fuel from rice straw. The process flow diagram for the pilot plant to produce edible sugars and solid biofuel from rice straw was depicted in Figure 4. Moreover, the quantitative flow sheet for edible sugar and biofuel from rice straw was illustrated in Figure 5. Concisely, 1000 kg rice straw can be converted to 100 kg edible sugar and 700 kg solid biofuel and recovered 90% and 95 – 98% for sulfuric acid and ethanol.
Fig. 3. Flowsheet for production of edible sugar and solid biofuel from rice straw

Fig. 4. Process flow sheet of the pilot plant for the production of edible sugars and solid biofuel from rice straw
Fig. 5. Quantitative flow sheet for the production of edible sugar and biofuel from rice straw

On the other hand, there are many losses during operations. For instance, losses of acid are mainly gaseous fumes during hydrolysis, losses of the lignin during the process, some of the sugars converted to furfural compounds remained with the acid, and not all sugar precipitated. Some of the sugar remains in ethanol.

The sugar production process was based on two-steps concentrated H₂SO₄ hydrolysis of rice straw followed by separation and purification of sugars. Moreover, ethanol was separated from acids by using a distillation unit. The hydrolyzer unit can convert 10 kg/h rice straw to sugars, and their final yield was 1 kg sugars per batch. Based on the recovery of 1000 kg rice straw to edible sugar and solid biofuel per month (working days are usually assumed 25 days per month), the constructed hydrolyzer unit can be used for four batches per day (i.e., convert 40 kg/day). Table 4 represents the design feature for edible sugar and solid biofuel production equipment from rice straw.

<table>
<thead>
<tr>
<th>Item</th>
<th>Equipment</th>
<th>Design Feature</th>
<th>The material of Const.</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Ethanol storage tank</td>
<td>(Cylindrical) Volume = 200 L</td>
<td>High-Density Polyethylene</td>
</tr>
<tr>
<td>2</td>
<td>Acid storage tank</td>
<td>(Cylindrical) Volume = 100 L</td>
<td>High-Density Polyethylene</td>
</tr>
<tr>
<td>3</td>
<td>Hydrolysis tank 1</td>
<td>(Cylindrical) Volume = 200 L</td>
<td>Antiacid bricks</td>
</tr>
<tr>
<td>4</td>
<td>Hydrolysis tank 2</td>
<td>(Cylindrical) Volume = 200 L</td>
<td>Iron coated by PVDF</td>
</tr>
<tr>
<td>5</td>
<td>Separator (distiller)</td>
<td>Batch system with A 5 K.W. heater Volume = 200 L</td>
<td>Iron coated by PVDF</td>
</tr>
<tr>
<td>6</td>
<td>Water evaporator</td>
<td>(Cylindrical) Volume = 200 L</td>
<td>Iron coated by PVDF</td>
</tr>
<tr>
<td>7</td>
<td>Squeezing machine</td>
<td>Capacity = 50 L/h</td>
<td>Iron coated by PVDF</td>
</tr>
<tr>
<td>8</td>
<td>Filtration device</td>
<td>Capacity = 50 L/h</td>
<td>Polypropylene filter</td>
</tr>
<tr>
<td>9</td>
<td>Neutralization tank</td>
<td>(Cylindrical) Volume = 200 L</td>
<td>High-Density Polyethylene</td>
</tr>
<tr>
<td>10</td>
<td>Spray dryer</td>
<td>Capacity = 20 L/h</td>
<td>Stainless steel or cast iron</td>
</tr>
</tbody>
</table>
4. CONCLUSION
An economical method to convert biomass to sugars and solid biofuel using a concentrated acid hydrolysis process was applied to construct the pilot plant scale. Similar trends were obtained by performing the rice straw’s hydrolysis in the pilot plant, like sugar and solid fuel yield. The produced sugars contain 77% xylose and can be used as natural diet sugars. Also, the produced solid fuel has a high calorific value of 6952 kJ/kg. The silica extracted from solid fraction can be considered a valuable by-product with 99% distribution > 1018 nm. Ultimately, the highly efficient recovery of acid (90%), ethanol (95-98%), and water recycling were achieved to increase the process’s economy. As expected, the production of edible sugars and solid fuels from rice straw uses concentrated sulfuric acid hydrolysis seems useful. Therefore, it is feasible to produce edible sugars and biofuel from lignocellulosic waste in the near future.

REFERENCES
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إنتاج سكريات صالحة للأكل من الكتلة الحية باستخدام وحدة نصف صناعي

الملخص:

تعتبر إنتاج المواد الكيميائية والوقود من الكتلة الحيوية تقنية إنتاج نظيف ولحمية البيئة. في هذه الدراسة، تم دراسة إنشاء عملية جديدة لتحويل الكتلة الحيوية إلى سكريات عالية النقاء ووقود حيوي صلب عن طريق التحليل المائي. في عملية إنتاج السكر، تم تحضير الكتلة النباتية إلى أصباغ الكرتونيكي، ومن ثم عملية الفصل والتقسيم المائي، ويتم فصل السكريات والالبانول بعدها التقطير. يمكن وحدة التحليل المائي المحمي تحقيق تحليل السكريات 1 كجم لكل دفعة. تم تحقيق طريقة اقتصادية لفصل السكريات عن طريق الترسب باستخدام الالبانول واسترجاع الحمض بكفاءة عالية (90%) والالبانول (98%) دون استخدام الرياح. أظهر تحليل كرموجرافى سائل قلي الأداء للتحليل المائي أنه يحتوي على 77% زئبق، والذي يمكن استخدامه كسكر طبيعي طبيبي. تم الحصول على إنتاج 70-100 كجم من السكريات الغذائية الطبيعية و 700 كجم من الوقود الحيوي الصلب (القيمة الحجازية 6952 كيلو جول / كجم) من 1000 كجم فض الأرز. يمكن اعتبار النتائج من الوحدة النصف صناعية كخطوة نحو الإنتاج على نطاق صناعي وتجاري.